# **Roundabout Model Calibration Issues and a Case Study**

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Pictures modified to show driving on the right-hand side of the road Rahmi Akçelik



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# **This paper**

- Issues related to calibration of models for analyzing roundabout capacity and performance discussed.
- A traffic model framework presented to help with assessment of traffic models in a general framework.
- While the discussion focuses on analytical models, the issues raised are also relevant to microsimulation models.
- Discussion on roundabout models should not concentrate on capacity alone, and instead, modeling requirements for estimating both capacity and performance (v/c ratio, delay, queue length, etc) should be considered together.
- Various aspects of field observations relevant to the calibration effort are discussed. These include issues related to the definition and measurement of capacity, delay and queue length, including the effect of unequal lane utilization.
- Delay criteria for level of service definition are also discussed



# **This paper**

- Two basic calibration methods that can be used for gap-acceptance and linear regression methods are described.
- Further aspects of model calibration discussed include
  - environment factor
  - adjustment for the arrival flow / circulating flow ratio
  - lane utilization factor
  - heavy vehicle factor
  - driver response time
  - parameters for operating cost, emissions and fuel consumption
- A case study is presented to compare capacity estimates from the gap-acceptance and linear-regression methods, including a calibration example





# **Model calibration**

- Effective use of models to analyze intersection capacity, performance and level of service may require significant calibration effort.
- The Highway Capacity Manual defines calibration as "The process of comparing model parameters with real-world data to ensure that the model realistically represents the traffic environment. The objective is to minimize the discrepancy between model results and measurements or observations."
- The nature of the model in use determines the calibration effort. Therefore, a good understanding of the basic premises of the model is an essential step in model calibration.





#### A Case Study: T-intersection roundabout (based on article by CHARD, UK)





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#### **Capacity results for the T-intersection roundabout**

App. ID	Approach Name	Total App. Flow (veh/h)	Circul. Flow (1) (pcu/h)	Critical Lane (2)	Critical Lane Flow (veh/h)	Total App. Capacity (veh/h)	Critical Lane capacity (veh/h)	Degree of saturation (v/c ratio)	Practical Spare Capacity (x <sub>p</sub> = 0.85)
			aaSIDRA: Single-lane circulating road and exclusive approach lanes						
W	Δrm Δ	800	733	1 (T)	400	1435	629	0.635	34%
s	Arm B	1600	400	1(1)	800	2167	984	0.813	5%
F	Arm C	1000	800	1(L)	800	1224	733	1 091	-22%
<b>-</b>		1000	000	· (⊑)	000			1.031	-22 /0
				Two-la	ne circula	aasid ating road ar	nd shared a	approach lane	S
W	Arm A	800	800	2 (TR)	431	1507	812	0.531	60%
S	Arm B	1600	400	2 (LR)	841	2050	1078	0.781	9%
Е	Arm C	1000	800	2 (LT)	537	1419	762	0.705	21%
			TRL (UK) Linear Regression Model: Same results for both lane arrangements						
W	Arm A	800	800	-	-	1490	-	0.537	58%
S	Arm B	1600	400	-	-	1771	-	0.904	-6%
E	Arm C	1000	800	-	-	1490	-	0.671	27%

(1) Circulating flows for two-lane circulating road are without any capacity constraint since all approach lanes are estimated to be undersaturated (both models).

(2) aaSIDRA approach degrees of saturation represent the critical lane degrees of saturation (L: Left, T: Through, R: Right). The TRL capacity model combines exclusive and shared lanes to obtain an average approach degree of saturation.





# **Comparisons**

- aaSIDRA estimates differ significantly for the single-lane and twolane circulating road cases
- The UK (TRL) model estimates for the two cases are identical.
- Assumptions of the "approach" method used in the UK (TRL) model are close to the case of *two-lane circulating road with shared* approach lanes, and therefore in close agreement with the aaSIDRA method.
- On the other hand, a large discrepancy is found between the two models in the case of single-lane circulating road with exclusive lanes.



# Comparisons

- aaSIDRA estimates of delay, operating cost, fuel consumption and CO<sub>2</sub> emission comparing the case of single-lane circulating road with exclusive lanes vs the case of two-lane circulating road with shared lanes showed that, considering annual values of one hour of traffic operation only, the difference between the two cases amounted to approximately:
  - o 9,000 person-hours of delay
  - US\$72,000 in operating cost
  - 14,000 L of fuel consumption
  - 34,000 kg of CO<sub>2</sub> emission per year.





## **Lane Utilization**

- Different methods have been used to measure and model capacities in terms of *level of aggregation*:
  - (i) *lane-by-lane* analysis as in aaSIDRA
  - (ii) analysis by *lane groups* as in the HCM, and
  - (iii) analysis by total *approach flows*, i.e. all movements in all approach lanes aggregated, as in the TRL method for roundabout capacity analysis
- A simple sum of lane capacity values calculated as the lane group or approach capacity is misleading in the case of lane underutilization since such an aggregate capacity value does not reflect the critical lane volume - capacity ratio, and therefore may underestimate delays and queue lengths significantly.
- It is important to carry out functional design to ensure balanced use of approach and circulating road lanes before detailed design of a roundabout (including use of bypass lanes, i.e. slip lanes and continuous lanes).







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### **Unequal lane use may be due to:**

- exclusive lanes as determined by lane marking and signing,
- path overlap on the circulating road due to poor roundabout design, and lack of circulating lane markings,
- a lane that discontinues at the downstream side due to a decreased number of lanes or parked vehicles (downstream short lane),
- a lane with a large proportion of traffic turning left or right at a downstream location (destination effect),
- some interference at the downstream side, e.g. vehicles merging from a slip lane with no clear give-way (yield) lane markings,
- a large number of heavy commercial vehicles or buses (moving or stopping) in the lane,
- turning vehicles in the lane subject to heavy pedestrian conflict at the exit,
- heavy interference by parking maneuvers (parking adjacent to the lane), or
- an approach short lane (e.g. a turn bay, or a limited queuing space due to parking upstream).



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# **Calibration parameters**

- The model input parameters representing driver behavior, vehicle characteristics, the intersection geometry and control need to be identified for the purpose of calibration.
- For roundabouts and other unsignalised intersections, gap-acceptance parameters (especially follow-up headway and critical gap) are the key parameters representing driver behavior.
- The overall roundabout geometry (configuration of approach roads, number of approach and circulating road lanes, allocation of lanes to movements) affects the capacity and performance directly.
- The gap-acceptance parameters as well as the approach and circulating road lane use are affected by the roundabout geometry as well as the overall demand flow levels and patterns.





# **Calibration methods**

- Modify the follow-up headway and critical gap values so that estimates of capacity, delay or queue length values match the observed values, as provided with the aaSIDRA method
- Modify the intercept value of the linear capacity circulating flow equation, as provided with the UK (TRL) linear regression method





## **Calibration of gap-acceptance parameters to match observed capacity**





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# Adjustment of the intercept of linear regression equation to match observed capacity





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#### **Model calibration process:**

#### aaSIDRA and other gap-acceptance methods

Observed parameters	Gap-acceptance parameters	Capacity	Delay or Queue Length
Gap- acceptance parameters	Specify observed gap-acceptance parameters.	Capacity estimate is modified by observed gap- acceptance parameters.	Affected by modified capacity estimate (indirect effect), and observed gap- acceptance parameters (direct effect).
Capacity	Specify modified gap-acceptance parameters to match observed capacity.	Observed capacity is achieved.	Affected by observed capacity (indirect effect), and modified gap- acceptance parameters (direct effect).
Delay or queue length	Specify modified gap-acceptance parameters to match observed delay or queue length.	Capacity estimate is affected via modified gap- acceptance parameters.	Observed delay or queue length is achieved using modified gap-acceptance parameters (direct effect) and the resulting modified capacity estimate (indirect effect).



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#### Model calibration process: UK and other linear regression methods

Observed parameters	Gap-acceptance parameters	Capacity	Delay or Queue Length
Capacity	Not applicable	Specify modified intercept to match observed capacity.	Affected by observed capacity (indirect effect).
Delay or queue length	Not applicable	Specify modified intercept to match observed delay or queue length. Capacity estimate is affected via modified intercept.	Observed delay or queue length is achieved using modified capacity estimate (indirect effect).





#### **Environment Factor**

**Higher capacity**: good visibility, more aggressive and alert driver attitudes (smaller response times), negligible pedestrian volumes, insignificant parking and heavy vehicle activity (goods vehicles, buses, trams stopping on approach roads).

Lower capacity: low visibility, relaxed driver attitudes (slower response times), high pedestrian volumes, significant parking and heavy vehicle activity (goods vehicles, buses, trams stopping on approach roads).





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#### **Adjustment Level for Arrival Flow / Circulation Flow Ratio**

In order to avoid underestimation of capacities at low circulating flows, aaSIDRA decreases the dominant lane follow-up headway as a function of the ratio of arrival (entry lane) flow to circulating flow.





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# **Excel application for model comparison - HCM single-lane roundabout example, WB approach:**

inscribed diameter = 36 m (118 ft), entry lane width = 4.0 m (13 ft), approach half width = 3.5 m (11.5 ft), turn radius = 26 m (84 ft), flare length = 20 m (66 ft), entry angle =  $30^{\circ}$ 

aaSIDRA model with default parameters: Environment Factor = 1.0, Medium entry flow adjustment, Medium O-D pattern effect



aaSIDRA model calibrated to match the HCM lower capacity model: Environment Factor = 1.15, Low entry flow adjustment, Medium O-D pattern effect





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# **Model Framework**

		ROA	D GEOMETRY EL	EMENTS	
VTS		APPROACHES (all lanes aggregated) LANE GROUPS (or "links")		LANES (or lane segments)	
EMEN	Individual vehicles			Micro-simulation	
	Platoons	Macro-si	Meso-simulation		
	Drive cycles			Micro-analytical	
RAF	Traffic flows	Macro-analytical	Meso-	analytical	
F	Speed-flow models		Macro-analytica	al	





# **About models**

- a simulation model can be microscopic, macroscopic or mesoscopic
- an analytical model can be microscopic, macroscopic or mesoscopic, and
- a simulation model can be deterministic or stochastic
- contrasting models as "empirical vs theoretical" (as frequently done in the literature in relation to roundabout capacity models) represents a simplistic view since most models have basis in traffic behavior theory and are empirical at the same time.







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# **Roundabout capacity and performance**

aaSIDRA used in the analyses reported in this paper employs an *empirical gap-acceptance method* to model roundabout capacity and performance. The model allows for the effects of *both roundabout geometry and driver behaviour*, and it incorporates effects of *priority reversal* (low critical gaps at high circulating flows), *priority emphasis* (unbalanced O-D patterns), and *unequal lane use* (both approach and circulating lanes).

**CAPACITY** can be measured as a *service rate* for each traffic *lane* in *undersaturated conditions* (v/c ratios less than 1) according to the HCM definition of capacity to represent "*prevailing conditions*". This is in contrast with measuring *approach* capacity in *oversaturated conditions*.





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# Australian roundabout survey data

used for calibrating the Australian

gap-acceptance based capacity and performance models

	Total entry	No. of	Average	Circul.	Inscribed	Entry	Conflict
	width	entry	entry lane	width	Diameter	radius	angle
	(ft)	lanes	width (ft)	(ft)	(ft)	(ft)	(°)
Minimum	12	1	10	21	52	13	0
Maximum	41	3	18	39	722	×	80
Average	27	2	13	31	183	128	29
15th percentile	21	2	11	26	93	33	0
85th percentile	34	3	15	39	230	131	50
Count	55	55	55	55	55	55	55
	Follow-up	Critical	Crit. Gap /	Circul.	Total	Dominant	Subdom.
	Follow-up Headway	Critical Gap	Crit. Gap / Fol. Hw	Circul. flow	Total entry flow	Dominant lane flow	Subdom. lane flow
	Follow-up Headway (s)	Critical Gap (s)	Crit. Gap / Fol. Hw Ratio	Circul. flow (veh/h)	Total entry flow (veh/h)	Dominant Iane flow (veh/h)	Subdom. lane flow (veh/h)
Minimum	Follow-up Headway (s) 0.80	Critical Gap (s) 1.90	Crit. Gap / Fol. Hw Ratio 1.09	Circul. flow (veh/h) 225	Total entry flow (veh/h) 369	Dominant lane flow (veh/h) 274	Subdom. lane flow (veh/h) 73
Minimum Maximum	Follow-up Headway (s) 0.80 3.55	Critical Gap (s) 1.90 7.40	Crit. Gap / Fol. Hw Ratio 1.09 3.46	Circul. flow (veh/h) 225 2648	Total entry flow (veh/h) 369 3342	Dominant lane flow (veh/h) 274 2131	Subdom. lane flow (veh/h) 73 1211
Minimum Maximum <mark>Average</mark>	Follow-up Headway (s) 0.80 3.55 2.04	Critical Gap (s) 1.90 7.40 3.45	Crit. Gap / Fol. Hw Ratio 1.09 3.46 1.75	Circul. flow (veh/h) 225 2648 1066	Total entry flow (veh/h) 369 3342 1284	Dominant lane flow (veh/h) 274 2131 796	Subdom. lane flow (veh/h) 73 1211 501
Minimum Maximum <mark>Average</mark> 15th percentile	Follow-up Headway (s) 0.80 3.55 2.04 1.32	Critical Gap (s) 1.90 7.40 3.45 2.53	Crit. Gap / Fol. Hw Ratio 1.09 3.46 1.75 1.26	Circul. flow (veh/h) 225 2648 1066 446	Total entry flow (veh/h) 369 3342 1284 690	Dominant lane flow (veh/h) 274 2131 796 467	Subdom. lane flow (veh/h) 73 1211 501 224
Minimum Maximum <mark>Average</mark> 15th percentile 85th percentile	Follow-up Headway (s) 0.80 3.55 2.04 1.32 2.65	Critical Gap (s) 1.90 7.40 3.45 2.53 4.51	Crit. Gap / Fol. Hw Ratio 1.09 3.46 1.75 1.26 2.31	Circul. flow (veh/h) 225 2648 1066 446 1903	Total entry flow (veh/h) 369 3342 1284 690 1794	Dominant lane flow (veh/h) 274 2131 796 467 1002	Subdom. lane flow (veh/h) 73 1211 501 224 732



#### **Data from roundabout capacity surveys at UK roundabouts** (indicating regression model bias)





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# **Examples of 'Conventional' and 'Offside Priority' roundabout designs used in capacity measurements for TRL (UK) linear regression model**



These old or experimental roundabout designs have not been used in Australia or USA



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# CAPACITY

- Capacity is the maximum sustainable flow rate that can be achieved under prevailing road, traffic and control conditions.
- Capacity is not a constant value.
- Capacity represents the service rate (queue clearance rate) in the performance functions, and therefore is relevant to both undersaturated and oversaturated conditions.
- Not to be confused with the maximum volume that the intersection can handle.
- Two distinct methods of *measuring capacity*:
  - (i) measuring departure (saturation) flow rates during saturated (queued) portions of unblocked periods of gap-acceptance cycles and the associated proportion of time available for queue discharge, and
  - (ii) measuring departure flow rates (volume counts) at the stop or give-way (yield) line under continuous queuing (saturated) conditions.



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# Conclusion

- Calibration effort usually focuses on making the best use of an available model in matching the estimates of capacity, delay, queue length, and other statistics produced by the model with values observed in the field.
- While such an effort can be successful in specific cases, such success does not guarantee the model validity in a general sense. This applies to all models, analytical and simulation.
- Discussion on the nature of models from the perspective of a general modeling framework is recommended in order to assess the capabilities of alternative models.
- Such discussion should not be limited to capacity or individual performance measures, but a more general evaluation of model capabilities should be undertaken.





# Disclaimer

The author is the developer of the aaSIDRA model, and comments presented in this paper regarding other models should be read with this in mind.

The comments about the TRL (UK) linear regression model are relevant to the original published model and are valid for software packages using that model only to the extent that the original model is used without modification to address the issues raised in this paper.





# **End of presentation**





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